

An Innovative Particle Swarm Optimization-Based Approach for GPR Microwave Imaging

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Abstract

This work presents an innovative microwave imaging technique for accurate and robust subsurface imaging. The proposed approach is based on the integration of a customized particle swarm optimization (*PSO*) algorithm within the iterative multi-scaling approach (*IMSA*), and exploits multiple frequency components extracted from ground penetrating radar (*GPR*) wideband data. The solution of the arising inverse scattering problem is yielded within a multi-frequency (*MF*) approach, allowing to exploit the intrinsic frequency diversity of *GPR* measurements in order to add information and mitigate the ill-posedness and non-linearity issues. Some numerical experiments are shown in order to assess the effectiveness of the proposed *MF-IMSA-PSO* method when dealing with the retrieval of unknown buried scatterers having different shape. Moreover, a comparison to a competitive state-of-the-art deterministic approach is shown, in order to highlight the benefits of exploiting a global optimization algorithm in minimizing the *MF* cost function.

1 Definitions

1.1 Glossary

- SF : Single-Frequency;
- FH : Frequency-Hopping;
- MF : Multi-Frequency;
- P : Swarm dimension;
- U : Total number of unknowns;
- S : Maximum number of $IMSA$ zooming steps;
- s^{best} : Last performed $IMSA$ zooming step ($s^{best} \leq S$);
- η_{th} : $IMSA$ zooming threshold;
- D_{inv} : Investigation domain;
- D_{obs} : Observation domain;
- L : Side of the investigation domain;
- N : Number of discretization cells in D_{ind} ;
- V : Number of views;
- M : Number of measurement points;
- F : Number of frequencies considered for the inversion;
- $\mathbf{r}^{(v)} = (x^{(v)}, y^{(v)})$: Coordinates of the v -th source ($v = 1, \dots, V$).
- $\mathbf{r}_m^{(v)} = (x_m^{(v)}, y_m^{(v)})$: Coordinates of the m -th measurement point for the v -th view v , ($m = 1, \dots, M$);
- $\varepsilon_{ra} = \frac{\varepsilon_a}{\varepsilon_0}$: Relative electric permittivity for the upper half-space ($y > 0$);
- σ_a : Conductivity for the upper half-space ($y > 0$);
- $\varepsilon_{rb} = \frac{\varepsilon_b}{\varepsilon_0}$: Background relative electric permittivity;
- σ_b : Background conductivity;
- $E_{inc}^{(v)}(\mathbf{r}_n; f)$: Measured internal incident field inside the n -th cell, for the v -th view at frequency f ;
- $\tilde{E}_{inc}^{(v)}(\mathbf{r}_n; f)$: Computed internal incident field inside the n -th cell, for the v -th view at frequency f ;
- $E_{scatt}^{(v)}(\mathbf{r}_m^{(v)}; f)$: Measured external scattered by the m -th measurement point, for the v -th view at frequency f ;
- $\tilde{E}_{scatt}^{(v)}(\mathbf{r}_m^{(v)}; f)$: Measured external scattered by the m -th measurement point, for the v -th view at frequency f .

1.2 Contrast function

The contrast function at frequency f is defined as

$$\tau(\mathbf{r}; f) = \frac{\varepsilon_{eq}(\mathbf{r}) - \varepsilon_{eqb}}{\varepsilon_0} = [\varepsilon_r(\mathbf{r}) - \varepsilon_{rb}] + j \left[\frac{\sigma_b - \sigma(\mathbf{r})}{2\pi f \varepsilon_0} \right]$$

where

- $\mathbf{r} = (x, y)$: position vector;
- $\Re\{\tau(\mathbf{r}; f)\} = [\varepsilon_r(\mathbf{r}) - \varepsilon_{rb}]$;
- $\Im\{\tau(\mathbf{r}; f)\} = \left[\frac{\sigma_b - \sigma(\mathbf{r})}{2\pi f \varepsilon_0} \right]$;
- $\varepsilon_{eq}(\mathbf{r}) = \varepsilon_0 \varepsilon_r(\mathbf{r}) - j \frac{\sigma(\mathbf{r})}{2\pi f}$;
- $\varepsilon_{eqb} = \varepsilon_0 \varepsilon_{rb} - j \frac{\sigma_b}{2\pi f}$;
- $\varepsilon_r(\mathbf{r})$: relative electric permittivity at position \mathbf{r} ;
- $\sigma(\mathbf{r})$: conductivity at position \mathbf{r} ;

NOTE: we assume that $\varepsilon_r(\mathbf{r})$ and $\sigma(\mathbf{r})$ are **not frequency dependent** (non-dispersive mediums).

1.2.1 Contrast function and reference frequency f_{ref} (MF approaches)

The contrast function at a generic frequency f can be expressed by means of the contrast function computed for a selected reference frequency

$$f = f_{ref} \tag{1}$$

as follows

$$\tau(\mathbf{r}; f) = \Re\{\tau(\mathbf{r}; f_{ref})\} + j \frac{f_{ref}}{f} \Im\{\tau(\mathbf{r}; f_{ref})\}. \tag{2}$$

This allows to reduce the number of unknowns when dealing with multi-frequency techniques, since we can just consider the contrast function at the reference frequency.

1.3 Cost function & unknowns

1.3.1 Multi-Frequency (*MF*) approaches

These approaches jointly consider data at F frequencies. The functional minimized by the inversion algorithm is defined as

$$\Phi(\mathbf{x}) = \Phi_{state}(\mathbf{x}) + \Phi_{data}(\mathbf{x}) \quad (3)$$

where $\Phi_{state}(\mathbf{x})$ and $\Phi_{data}(\mathbf{x})$ are respectively the data and state terms of the cost function, defined as

$$\Phi_{state}(\mathbf{x}) = \frac{\sum_{j=1}^F \sum_{v=1}^V \sum_{n=1}^N \left| E_{inc}^{(v)}(\mathbf{r}_n; f_j) - \tilde{E}_{inc}^{(v)}(\mathbf{r}_n; f_j) \right|^2}{\sum_{j=1}^F \sum_{v=1}^V \sum_{n=1}^N \left| E_{inc}^{(v)}(\mathbf{r}_n; f_j) \right|^2} \quad (4)$$

$$\Phi_{data} = \frac{\sum_{j=1}^F \sum_{v=1}^V \sum_{m=1}^M \left| E_{scatt}^{(v)}(\mathbf{r}_m^{(v)}; f_j) - \tilde{E}_{scatt}^{(v)}(\mathbf{r}_m^{(v)}; f_j) \right|^2}{\sum_{j=1}^F \sum_{v=1}^V \sum_{m=1}^M \left| E_{scatt}^{(v)}(\mathbf{r}_m^{(v)}; f_j) \right|^2} \quad (5)$$

The unknowns of the inversion problem are

$$\mathbf{x} = \left\{ \tau(\mathbf{r}; f_{ref}); E_{tot}^{(v)}(\mathbf{r}_n; f_j) \right\} \quad n = 1, \dots, N; v = 1, \dots, V; j = 1, \dots, F. \quad (6)$$

The total number of unknowns for *MF*-based approaches is then given by

$$U_{MF} = 2N(1 + VF). \quad (7)$$

1.4 Reconstruction errors

The following integral error is defined

$$\Xi_{reg} = \frac{1}{N_{reg}} \sum_{n=1}^{N_{reg}} \frac{|\tau_n^{act} - \tau_n^{rec}|}{|\tau_n^{act} + 1|} \quad (8)$$

where *reg* indicates if the error computation covers

- the overall investigation domain ($reg \Rightarrow tot$),
- the actual scatterer support ($reg \Rightarrow int$),
- or the background region ($reg \Rightarrow ext$).

2 Numerical Validation

2.1 O-Shaped object ($\varepsilon_{r,obj} = 5.0$, $\sigma_{obj} = 10^{-3}$ [S/m])

2.1.1 Parameters

Background

Inhomogeneous and nonmagnetic background composed by two half spaces

- Upper half space ($y > 0$ - air): $\varepsilon_{ra} = 1.0$, $\sigma_a = 0.0$;
- Lower half space ($y < 0$ - soil): $\varepsilon_{rb} = 4.0$, $\sigma_b = 10^{-3}$ [S/m];

Investigation domain (D_{inv})

- Side: $L_{D_{inv}} = 0.8$ [m];
- Barycenter: $(x_{bar}^{D_{inv}}, y_{bar}^{D_{inv}}) = (0.00, -0.4)$ [m];

Time-Domain forward solver (*FDTD - GPRMax2D*)

- Side of the simulated domain: $L = 6$ [m];
- Number of cells: $N^{FDTD} = 750 \times 750 = 5.625 \times 10^5$;
- Side of the *FDTD* cells $l^{FDTD} = 0.008$ [m];
- Simulation time window: $T^{FDTD} = 20 \times 10^{-9}$ [sec];
- Time step: $\Delta t^{FDTD} = 1.89 \times 10^{-11}$ [sec];
- Number of time samples: $N_t^{FDTD} = 1060$;
- Boundary conditions: perfectly matched layer (*PML*);
- Source type: Gaussian mono-cycle (first Gaussian pulse derivative, called “Ricker” in *GPRMax2D*)
 - Central frequency: $f_0 = 300$ [MHz];
 - Source amplitude: $A = 1.0$ [A];

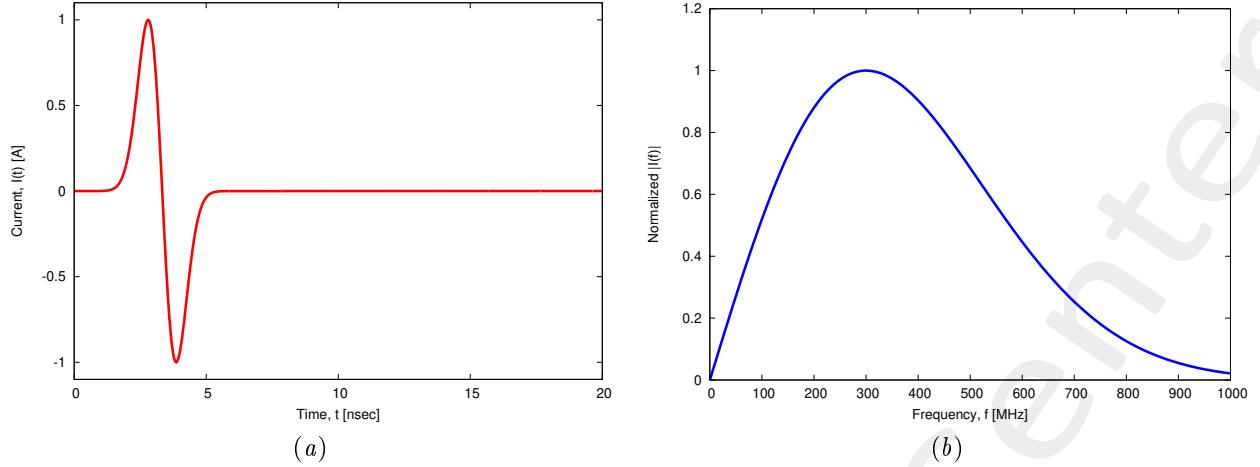


Figure 1: *GPRMax2D* excitation signal. (a) Time pulse, (b) normalized frequency spectrum.

Frequency parameters

- Frequency range: $f \in [f_{min}, f_{max}] = [200.0, 600.0]$ [MHz] (-3 [dB] bandwidth of the Gaussian Monocycle excitation centered at $f_0 = 300$ [MHz]);
- Frequency step: $\Delta f = 100$ [MHz] ($F = 5$ frequency steps in $[f_{min}, f_{max}]$);

| f [MHz] | λ_a [m] | λ_b [m] | f^* [MHz] |
|-----------|-----------------|-----------------|-------------|
| 200.0 | 1.50 | 0.75 | 200.5 |
| 300.0 | 1.00 | 0.50 | 297.6 |
| 400.0 | 0.75 | 0.37 | 401.1 |
| 500.0 | 0.60 | 0.30 | 498.1 |
| 600.0 | 0.50 | 0.25 | 601.6 |

Table 1: Considered frequencies and corresponding wavelength in the upper medium (λ_a , free space) and in the lower medium (λ_b , soil). f^* is the nearest frequency sample available from transformed time-domain data, and represents the real frequency considered by the inversion algorithm.

Scatterer

- Type: O-shaped;
- Barycenter: $(x_{obj}, y_{obj}) = (0.12, -0.36)$ [m];
- Side (external): $L_{obj,x} = L_{obj,y} = 0.24$ [m];
- Electromagnetic properties: $\varepsilon_{r,obj} = 5.0$, $\sigma_{obj} = 10^{-3}$ [S/m] ($\sigma_{obj} = \sigma_b$);
- Contrast function: $\tau = 1.0 + j0.0$

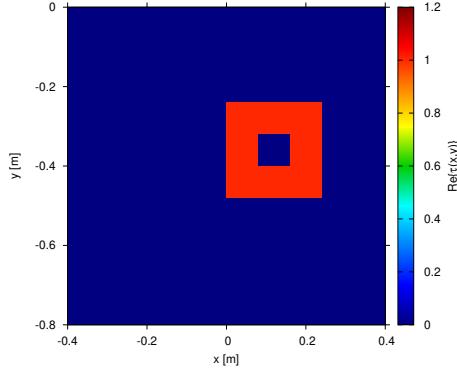


Figure 2: Actual object ($\tau = 1.0$).

Measurement setup

- Considered frequency: $f_{min} = 200$ [MHz], $\lambda_b = 0.75$ [m].¹
- $\#DoFs = 2ka = \frac{2\pi}{\lambda_b}L\sqrt{2} = \frac{2\pi}{0.75}0.8\sqrt{2} \simeq 9.5$;
- Number of views (sources): $V = 10$;
 - $\min\{x_v\} = -0.5$ [m], $\max\{x_v\} = 0.5$ [m];
 - height: $y_v = 0.1$ [m], $\forall v = 1, \dots, V$;
- Number of measurement points: $M = 9$;
 - $\min\{x_m\} = -0.5$ [m], $\max\{x_m\} = 0.5$ [m];
 - height: $y_m = 0.1$ [m], $\forall m = 1, \dots, M$;

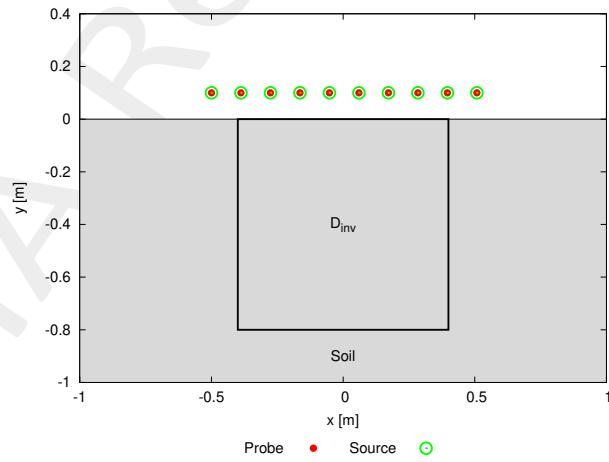


Figure 3: Location of the measurement points ($M = 9$) and of the sources ($V = 10$). Only one source is active for each view.

Inverse solver parameters

- Shared parameters

¹NOTE: This choice is done in order to keep the number of unknowns lower than 5000.

- Number of unknowns: $U = 2N(1 + VF) = 4998$;
- Weight of the state term of the functional: 1.0;
- Weight of the data term of the functional: 1.0;
- Weight of the penalty term of the functional: 0.0;
- Convergence threshold: 10^{-10} ;
- Variable ranges:

$$* \varepsilon_r \in [4.0, 5.2], \sigma \in [8.0 \times 10^{-4}, 1.2 \times 10^{-3}] [\text{S/m}];$$

$$* \Re\{E_{tot}^{int}\} \in [-8, 8], \Im\{E_{tot}^{int}\} \in [-8, 8];$$

- Degrees of freedom:

$$* \text{ Considered frequency: } f_{min} = 200 \text{ [MHz]}, \lambda_b = 0.75 \text{ [m]};$$

$$* \frac{(2ka)^2}{2} = \frac{\left(2 \times \frac{2\pi}{\lambda_b} \times \frac{L\sqrt{2}}{2}\right)^2}{2} = 4\pi^2 \left(\frac{L}{\lambda_b}\right)^2 = 4\pi^2 \left(\frac{0.8}{0.75}\right)^2 \simeq 44.87;$$

- Number of cells: $N = 49 = 7 \times 7$;
- Maximum number of *IMSA* steps: $S = 4$;
- Side ratio threshold: $\eta_{th} = 0.2$;

- ***MF – IMSA – PSO parameters***

- Maximum number of iterations: $I = 20000$;
- Swarm dimension: $P = \frac{5}{100} \times U = 250$;
- $C_1 = C_2 = 2.0$;
- Inertial weight: $w = 0.4$;
- Velocity clamping: enabled;

- ***MF – IMSA – CG parameters***

- Maximum number of iterations: $I = 200$;

Signal to noise ratio (on $E_{tot}(t)$)

- $SNR = \{50, 40, 30, 20\} \text{ [dB]} + \text{Noiseless data.}$

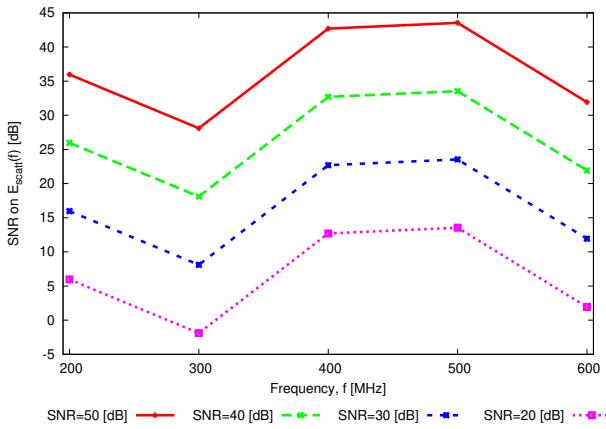


Figure 4: Signal to noise ratio (SNR [dB]) computed on the external scattered field in frequency domain for each considered frequency and for each input SNR on the measured total field in time-domain.

| SNR on $E_{tot}(t)$ [dB] | Av. SNR on $E_{scatt}(f)$ [dB] |
|--------------------------|--------------------------------|
| 50 | 36.4 |
| 40 | 26.4 |
| 30 | 16.4 |
| 20 | 6.4 |

Table 2: Average SNR measured on the scattered field in frequency domain.

2.1.2 $MF - IMSA - PSO$ vs. $MF - IMSA - CG$: Final reconstructions

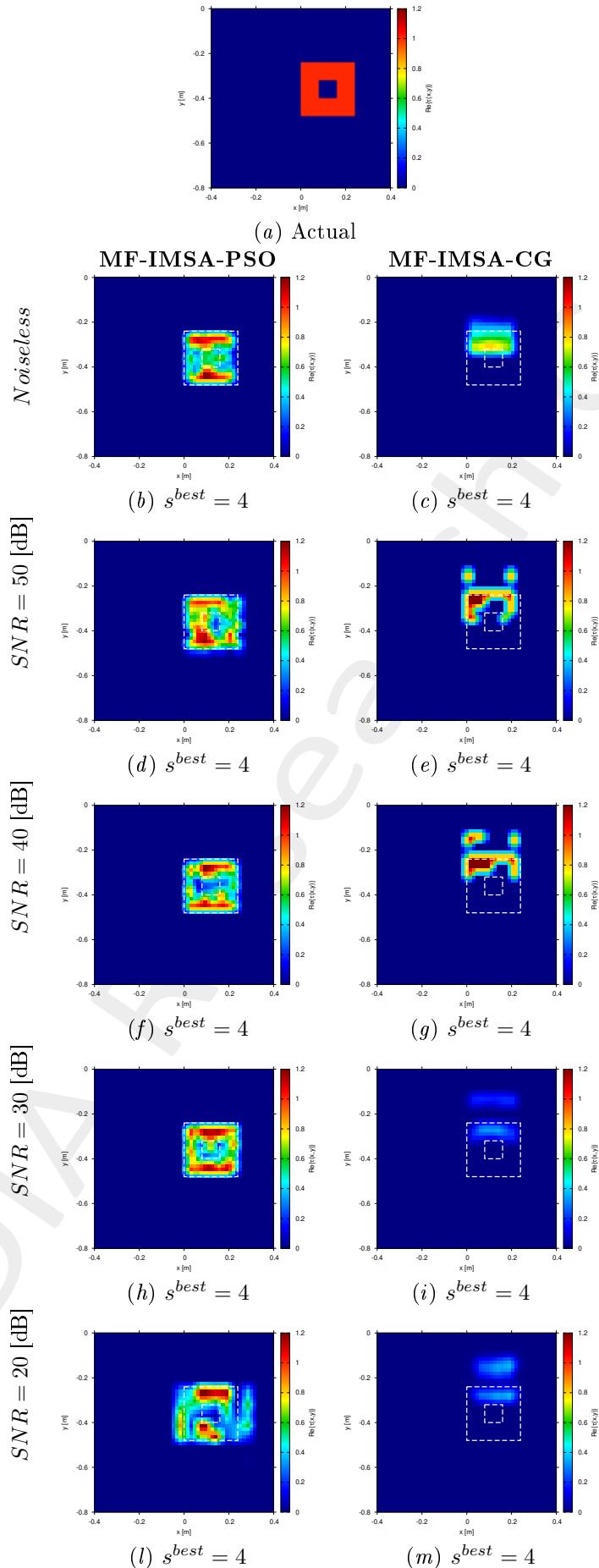


Figure 5: $MF - IMSA - PSO$ vs. $MF - IMSA - CG$: Retrieved dielectric profiles at the $IMSA$ convergence step (s^{best}).

2.1.3 $MF - IMSA - PSO$: Intermediate reconstructions

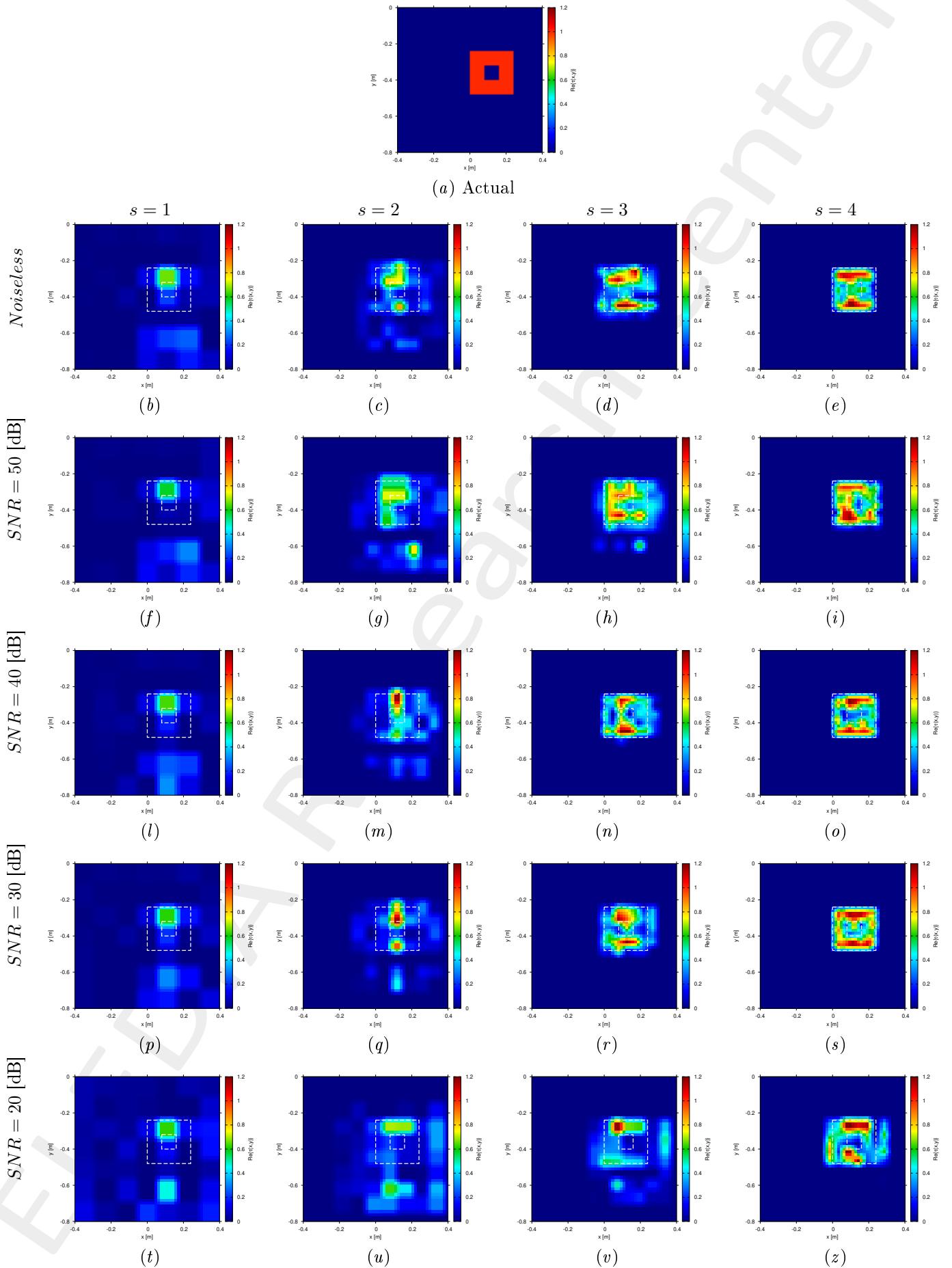


Figure 6: $MF - IMSA - PSO$: Retrieved dielectric profiles at each $IMSA$ step.

2.1.4 $MF - IMSA - CG$: Intermediate reconstructions

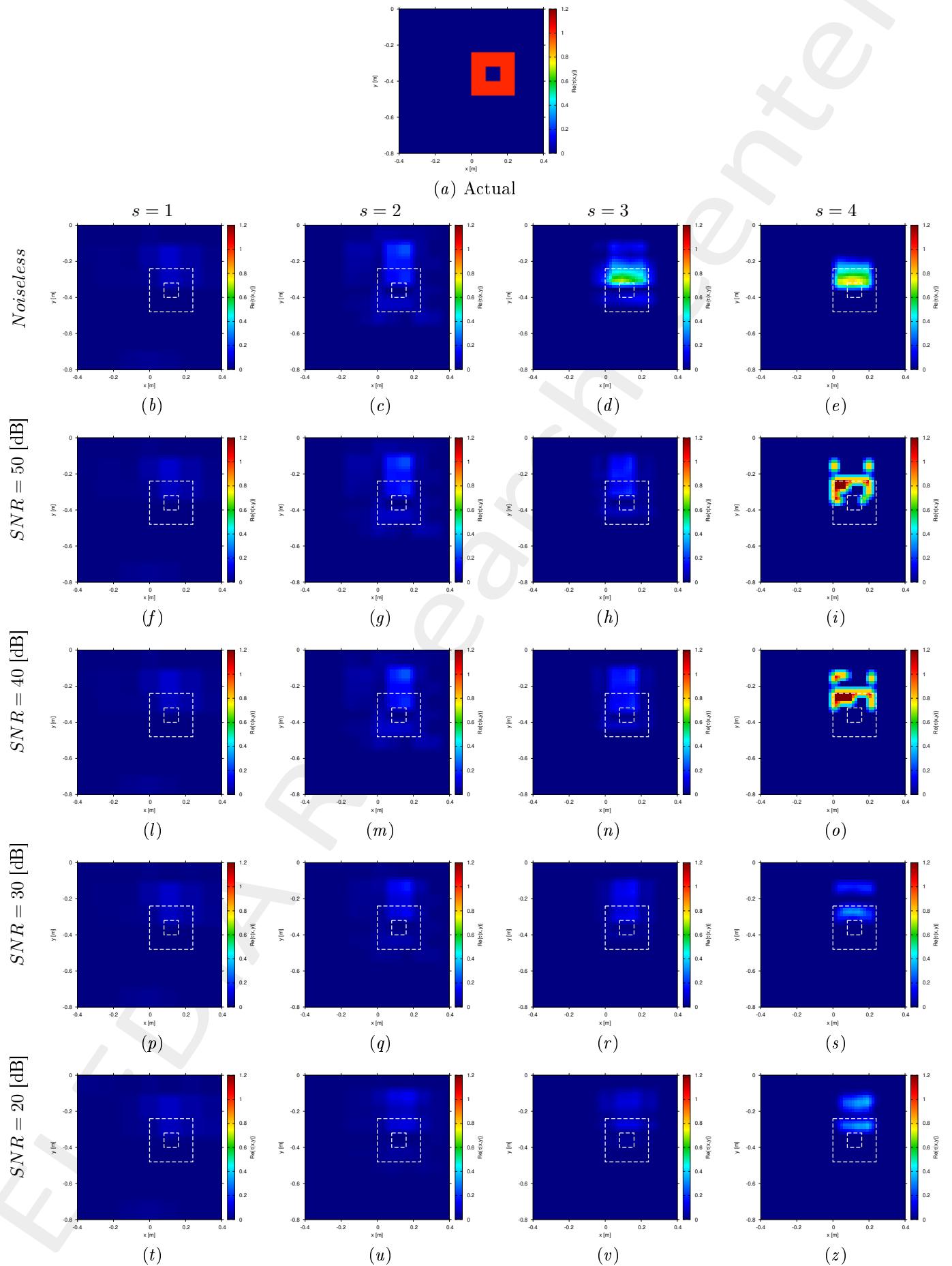


Figure 7: $MF - IMSA - CG$: Retrieved dielectric profiles at each *IMSA* step.

2.1.5 Reconstruction errors

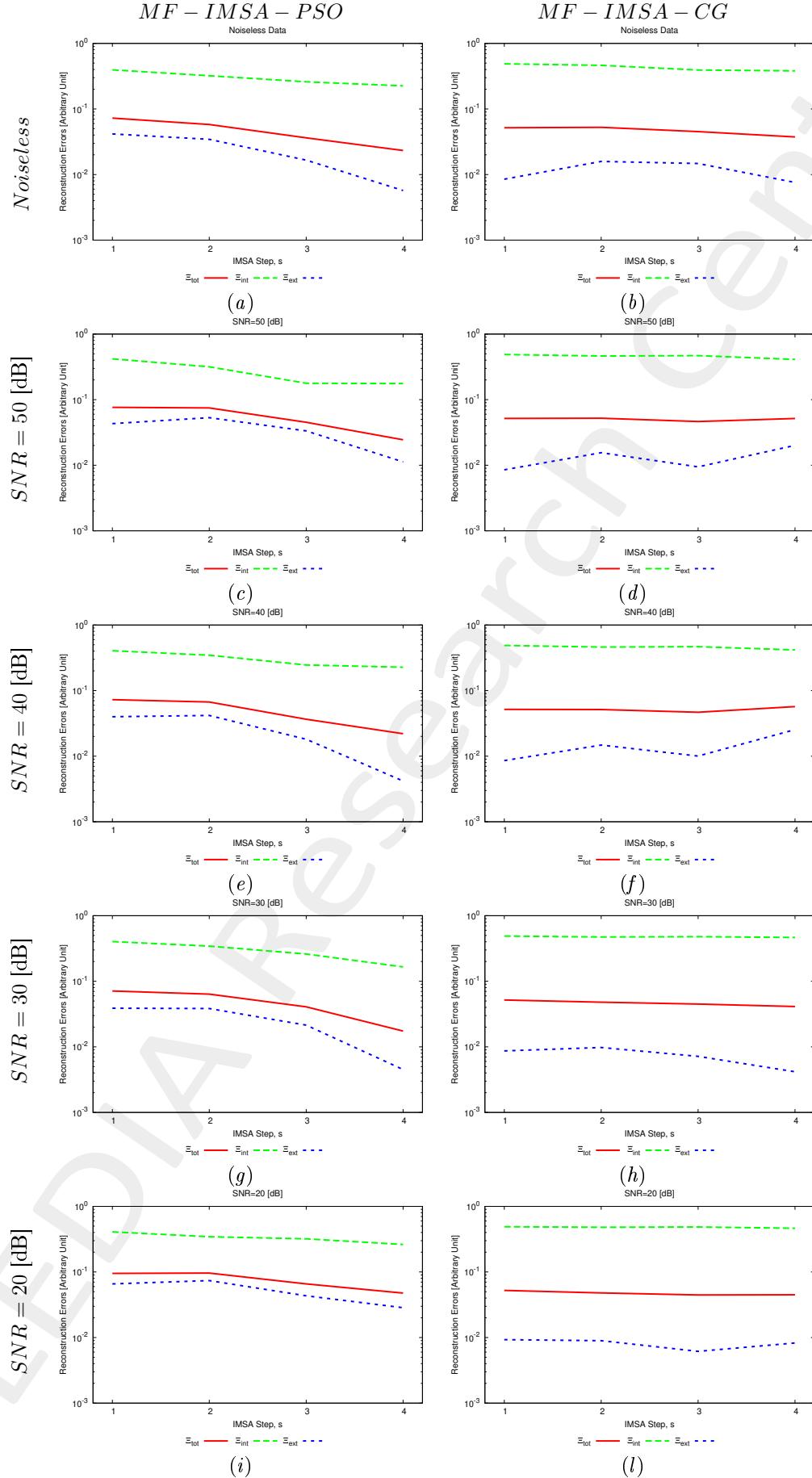


Figure 8: *MF - IMSA - PSO* vs. *MF - IMSA - CG*: Reconstruction error evolution.

2.1.6 Evolution of the cost function

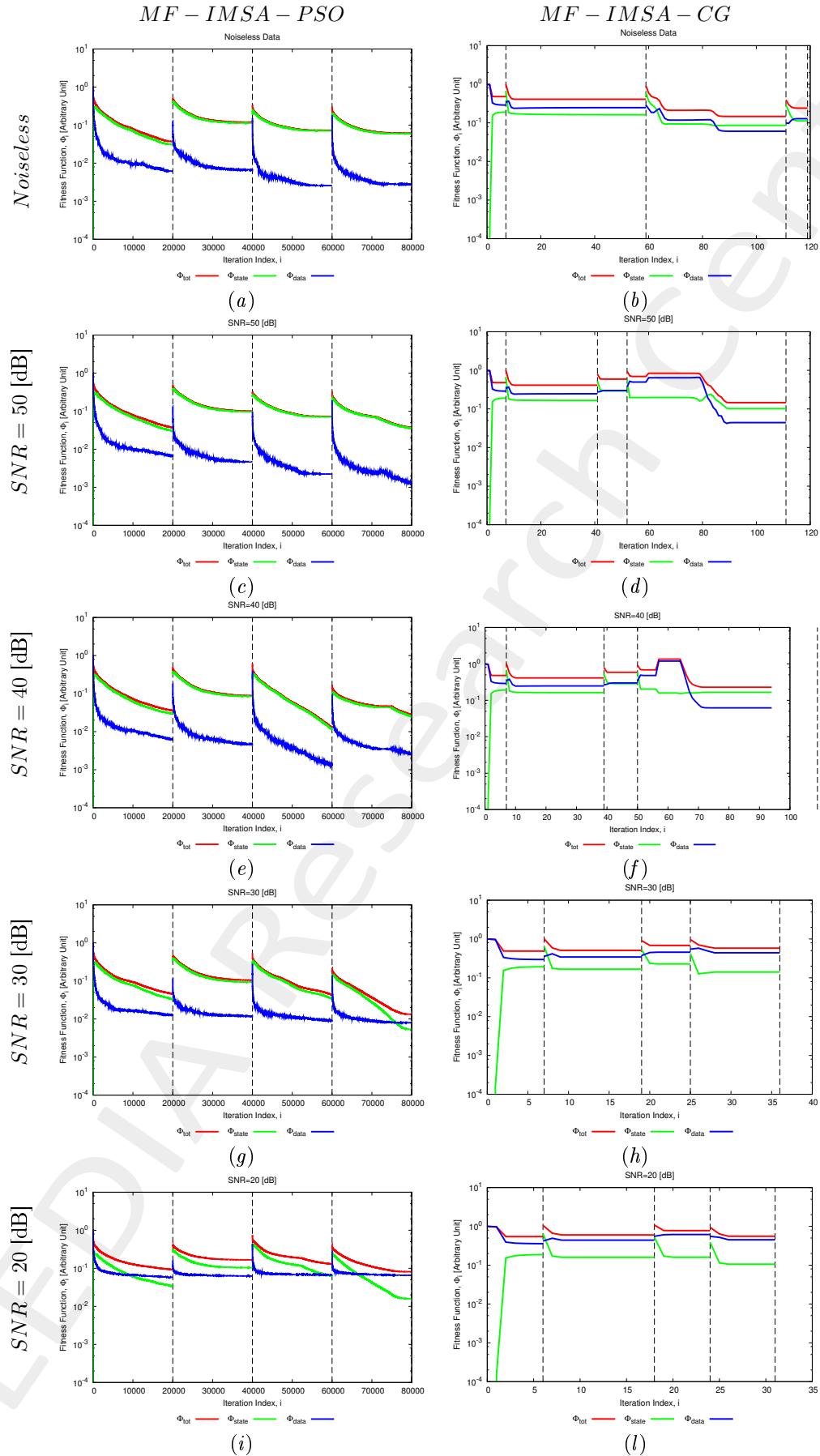


Figure 9: *MF - IMSA - PSO* vs. *MF - IMSA - CG*: Evolution of the cost function.

2.2 Circular object ($\varepsilon_{r,obj} = 5.0$, $\sigma_{obj} = 10^{-3}$ [S/m])

2.2.1 Parameters

Background

Inhomogeneous and nonmagnetic background composed by two half spaces

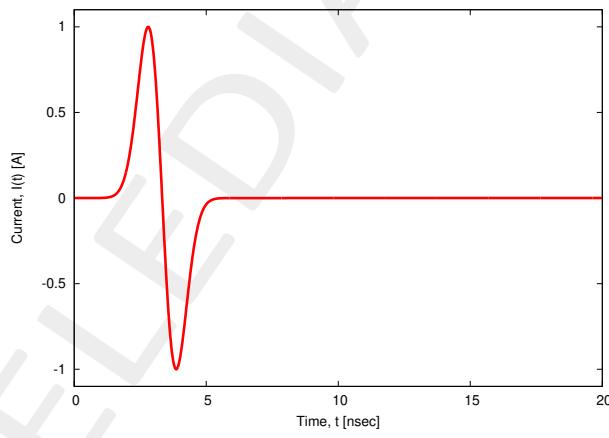
- Upper half space ($y > 0$ - air): $\varepsilon_{ra} = 1.0$, $\sigma_a = 0.0$;
- Lower half space ($y < 0$ - soil): $\varepsilon_{rb} = 4.0$, $\sigma_b = 10^{-3}$ [S/m];

Investigation domain (D_{inv})

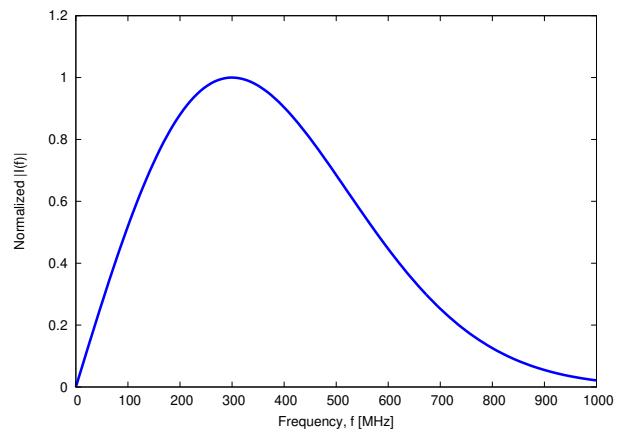
- Side: $L_{D_{inv}} = 0.8$ [m];
- Barycenter: $(x_{bar}^{D_{inv}}, y_{bar}^{D_{inv}}) = (0.00, -0.4)$ [m];

Time-Domain forward solver ($FDTD$ - $GPRMax2D$)

- Side of the simulated domain: $L = 6$ [m];
- Number of cells: $N^{FDTD} = 750 \times 750 = 5.625 \times 10^5$;
- Side of the $FDTD$ cells $l^{FDTD} = 0.008$ [m];
- Simulation time window: $T^{FDTD} = 20 \times 10^{-9}$ [sec];
- Time step: $\Delta t^{FDTD} = 1.89 \times 10^{-11}$ [sec];
- Number of time samples: $N_t^{FDTD} = 1060$;
- Boundary conditions: perfectly matched layer (PML);
- Source type: Gaussian mono-cycle (first Gaussian pulse derivative, called “Ricker” in $GPRMax2D$)
 - Central frequency: $f_0 = 300$ [MHz];
 - Source amplitude: $A = 1.0$ [A];



(a)



(b)

Figure 10: $GPRMax2D$ excitation signal. (a) Time pulse, (b) normalized frequency spectrum.

Frequency parameters

- Frequency range: $f \in [f_{min}, f_{max}] = [200.0, 600.0]$ [MHz] (-3 [dB] bandwidth of the Gaussian Monocycle excitation centered at $f_0 = 300$ [MHz]);
- Frequency step: $\Delta f = 100$ [MHz] ($F = 5$ frequency steps in $[f_{min}, f_{max}]$);

| f [MHz] | λ_a [m] | λ_b [m] | f^* [MHz] |
|-----------|-----------------|-----------------|-------------|
| 200.0 | 1.50 | 0.75 | 200.5 |
| 300.0 | 1.00 | 0.50 | 297.6 |
| 400.0 | 0.75 | 0.37 | 401.1 |
| 500.0 | 0.60 | 0.30 | 498.1 |
| 600.0 | 0.50 | 0.25 | 601.6 |

Table 3: Considered frequencies and corresponding wavelength in the upper medium (λ_a , free space) and in the lower medium (λ_b , soil). f^* is the nearest frequency sample available from transformed time-domain data, and represents the real frequency considered by the inversion algorithm.

Scatterer

- Type: Circular;
- Barycenter: $(x_{obj}, y_{obj}) = (-0.16, -0.4)$ [m];
- Radius: $r_{obj} = 0.08$ [m];
- Electromagnetic properties: $\varepsilon_{r,obj} = 5.0$, $\sigma_{obj} = 10^{-3}$ [S/m] ($\sigma_{obj} = \sigma_b$);
- Contrast function: $\tau = 1.0 + j0.0$

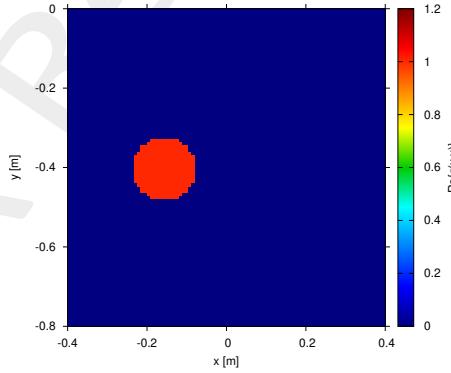


Figure 11: Actual object ($\tau = 1.0$).

Measurement setup

- Considered frequency: $f_{min} = 200$ [MHz], $\lambda_b = 0.75$ [m]. ²
- $\#DoFs = 2ka = \frac{2\pi}{\lambda_b} L \sqrt{2} = \frac{2\pi}{0.75} 0.8 \sqrt{2} \simeq 9.5$;
- Number of views (sources): $V = 10$;

²**NOTE:** This choice is done in order to keep the number of unknowns lower than 5000.

- $\min\{x_v\} = -0.5$ [m], $\max\{x_v\} = 0.5$ [m];
- height: $y_v = 0.1$ [m], $\forall v = 1, \dots, V$;
- Number of measurement points: $M = 9$;
- $\min\{x_m\} = -0.5$ [m], $\max\{x_m\} = 0.5$ [m];
- height: $y_m = 0.1$ [m], $\forall m = 1, \dots, M$;

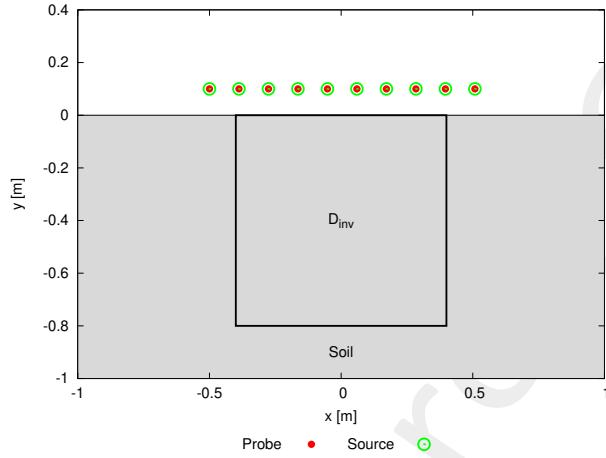


Figure 12: Location of the measurement points ($M = 9$) and of the sources ($V = 10$). Only one source is active for each view.

Inverse solver parameters

- Shared parameters
 - Number of unknowns: $U = 2N(1 + VF) = 4998$;
 - Weight of the state term of the functional: 1.0;
 - Weight of the data term of the functional: 1.0;
 - Weight of the penalty term of the functional: 0.0;
 - Convergence threshold: 10^{-10} ;
 - Variable ranges:
 - * $\varepsilon_r \in [4.0, 5.2]$, $\sigma \in [8.0 \times 10^{-4}, 1.2 \times 10^{-3}]$ [S/m];
 - * $\Re\{E_{tot}^{int}\} \in [-8, 8]$, $\Im\{E_{tot}^{int}\} \in [-8, 8]$;
 - Degrees of freedom:
 - * Considered frequency: $f_{min} = 200$ [MHz], $\lambda_b = 0.75$ [m];
 - * $\frac{(2ka)^2}{2} = \frac{\left(2 \times \frac{2\pi}{\lambda_b} \times \frac{L\sqrt{2}}{2}\right)^2}{2} = 4\pi^2 \left(\frac{L}{\lambda_b}\right)^2 = 4\pi^2 \left(\frac{0.8}{0.75}\right)^2 \simeq 44.87$;
 - Number of cells: $N = 49 = 7 \times 7$;
 - Maximum number of IMSA steps: $S = 4$;

- Side ratio threshold: $\eta_{th} = 0.2$;
- ***MF – IMSA – PSO parameters***
 - Maximum number of iterations: $I = 20000$;
 - Swarm dimension: $P = \frac{5}{100} \times U = 250$;
 - $C_1 = C_2 = 2.0$;
 - Inertial weight: $w = 0.4$;
 - Velocity clamping: enabled;
- ***MF – IMSA – CG parameters***
 - Maximum number of iterations: $I = 200$;

Signal to noise ratio (on $E_{tot}(t)$)

- $SNR = \{50, 40, 30, 20\}$ [dB] + Noiseless data.

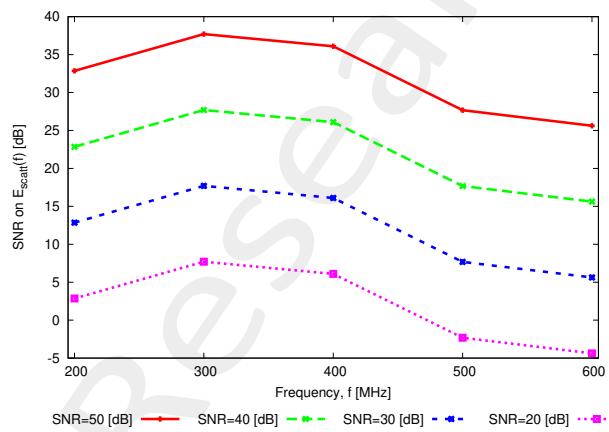


Figure 13: Signal to noise ratio (SNR [dB]) computed on the external scattered field in frequency domain for each considered frequency and for each input SNR on the measured total field in time-domain.

| SNR on $E_{tot}(t)$ [dB] | Av. SNR on $E_{scatt}(f)$ [dB] |
|--------------------------|--------------------------------|
| 50 | 32 |
| 40 | 22 |
| 30 | 12 |
| 20 | 2 |

Table 4: Average SNR measured on the scattered field in frequency domain.

2.2.2 $MF - IMSA - PSO$ vs. $MF - IMSA - CG$: Final reconstructions

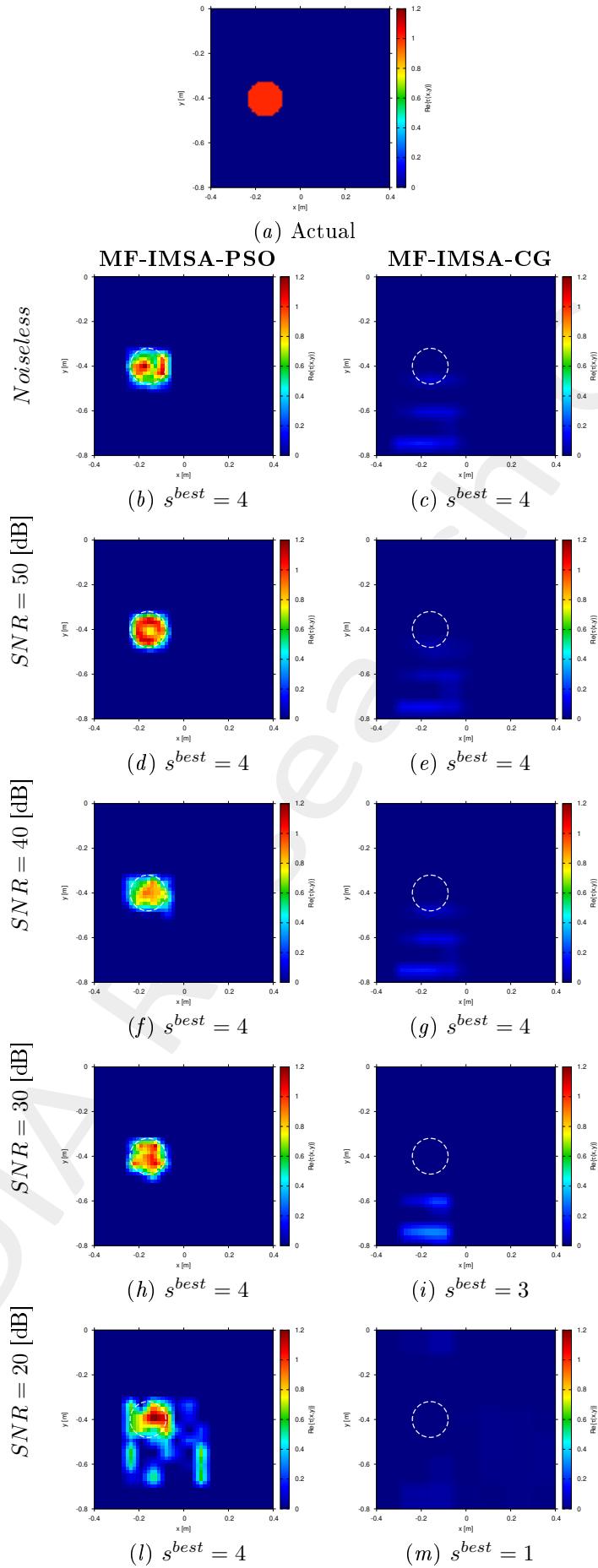


Figure 14: $MF - IMSA - PSO$ vs. $MF - IMSA - CG$: Retrieved dielectric profiles at the $IMSA$ convergence step (s^{best}).

2.2.3 $MF - IMSA - PSO$: Intermediate reconstructions

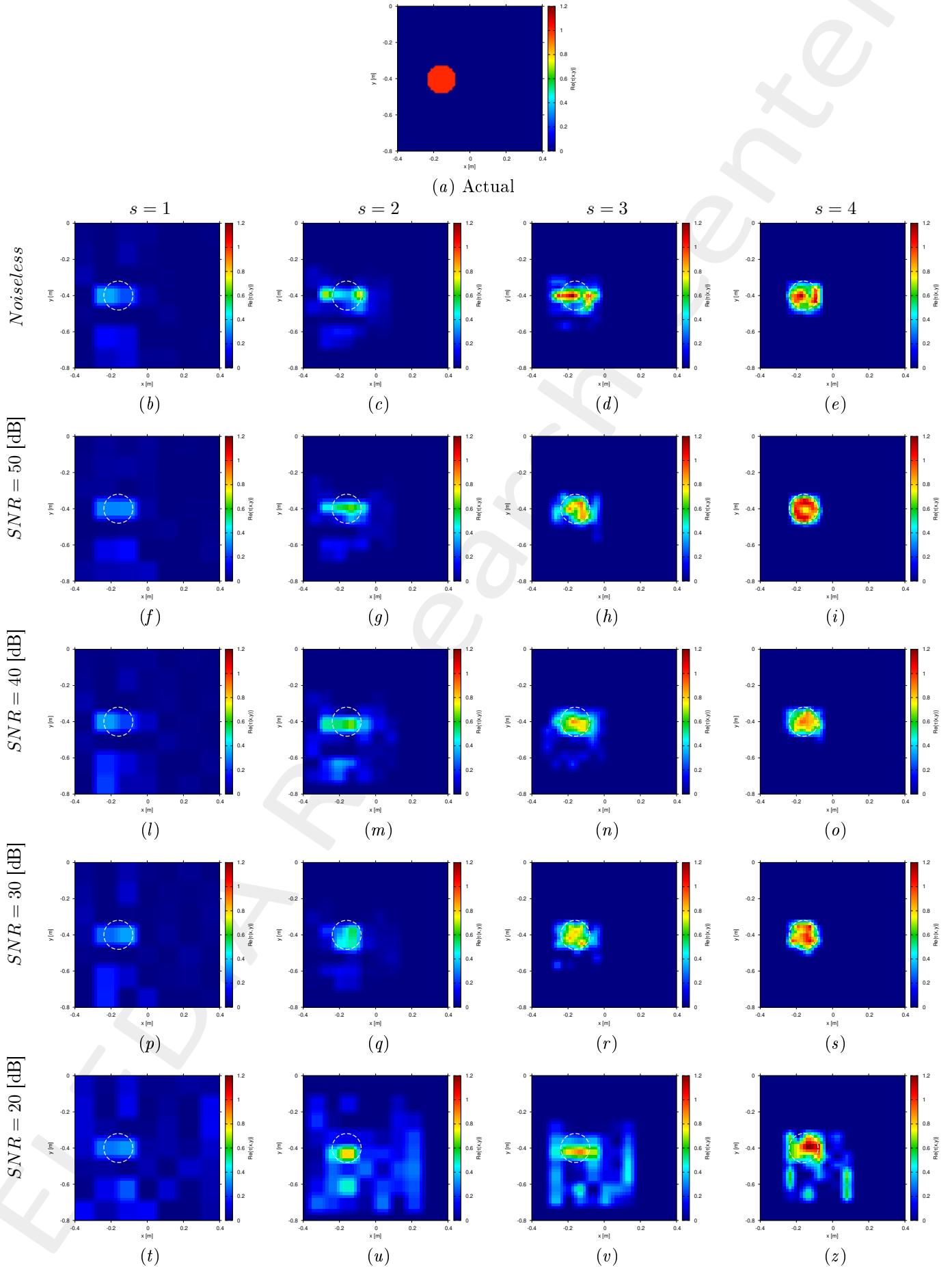


Figure 15: $MF - IMSA - PSO$: Retrieved dielectric profiles at each $IMSA$ step.

2.2.4 $MF - IMSA - CG$: Intermediate reconstructions

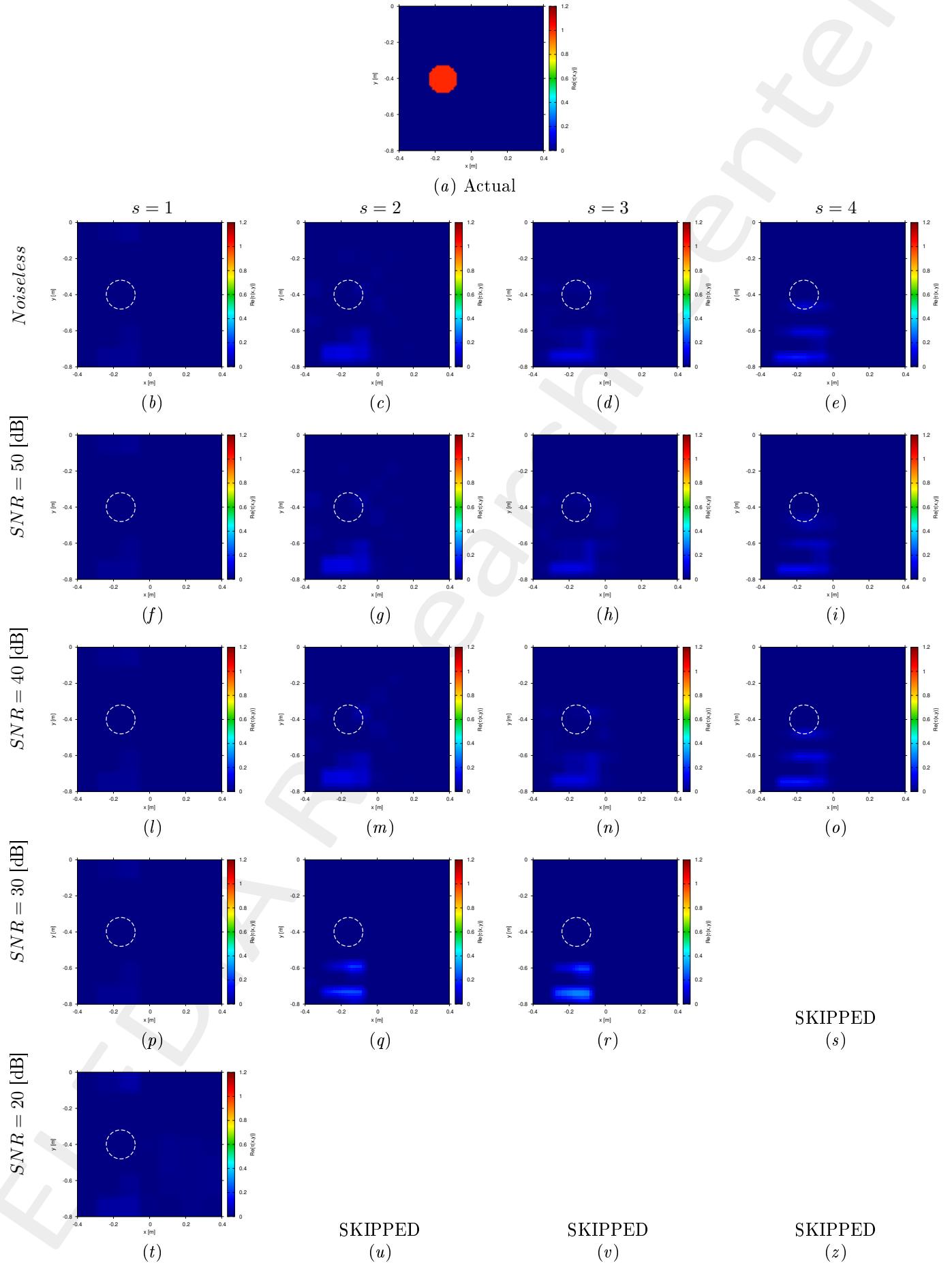


Figure 16: $MF - IMSA - CG$: Retrieved dielectric profiles at each $IMSA$ step.

2.2.5 Reconstruction errors

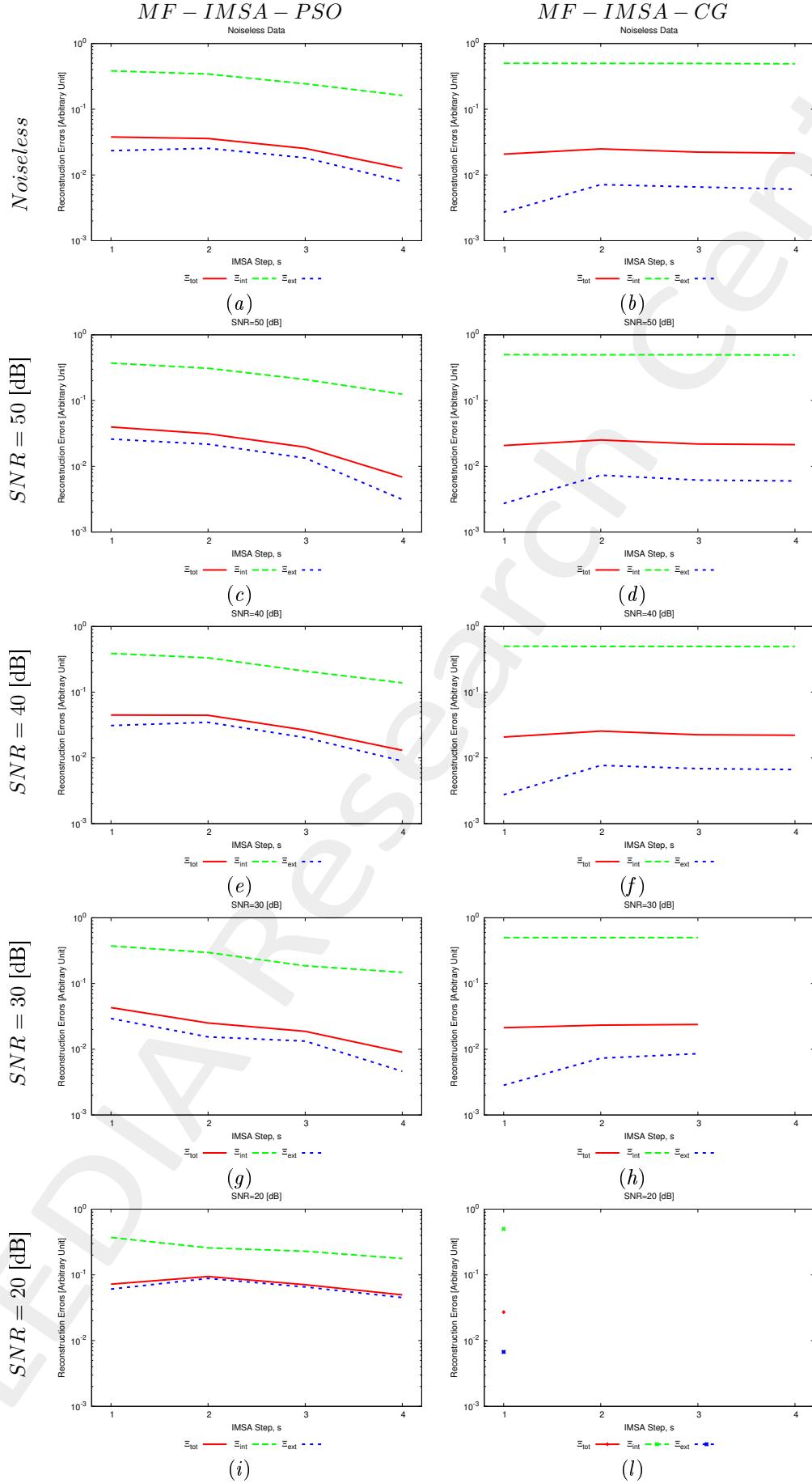


Figure 17: *MF - IMSA - PSO* vs. *MF - IMSA - CG*: Reconstruction error evolution.

2.2.6 Evolution of the cost function

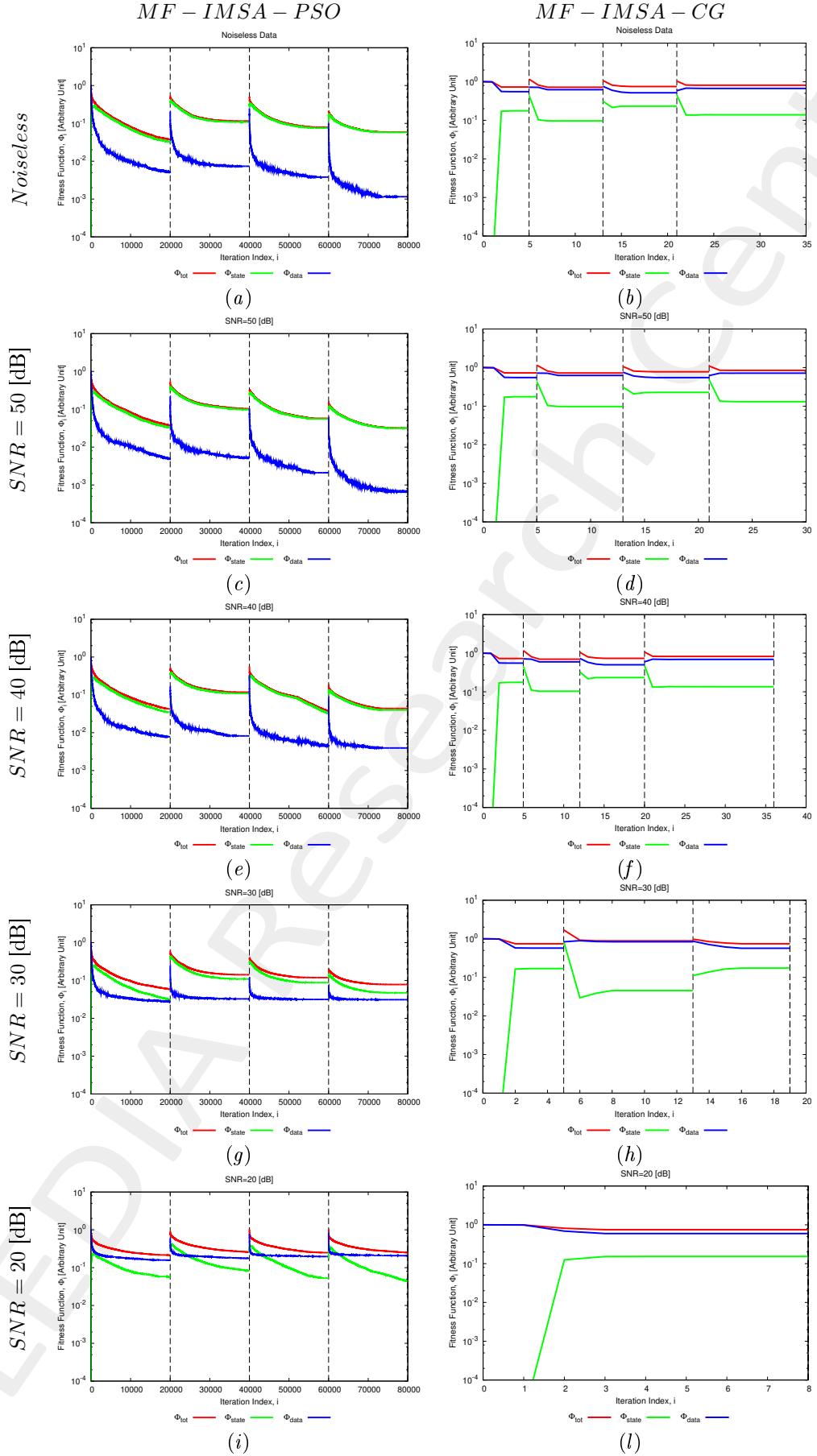


Figure 18: *MF - IMSA - PSO* vs. *MF - IMSA - CG*: Evolution of the cost function.

3 Conclusions

The reported numerical validation indicates that

- The $MF - IMSA - PSO$ provides better reconstruction with respect to the $MF - IMSA - CG$ thanks to the exploitation of a stochastic global search algorithm;
- The $MF - IMSA - PSO$ provides accurate results also when data is blurred with a non-negligible amount of noise;
- The $MF - IMSA - PSO$ is able to provide accurate reconstructions for objects of different size and shape.

More information on the topics of this document can be found in the following list of references.

References

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