A Pulse-Shifting Strategy applied to the Synthesis of Directive Time-modulated Linear Arrays

L. Poli, P. Rocca, A. Massa

Abstract

This report deals with the minimization of the amount of sideband radiation on time-modulated linear arrays by taking advantage of the directive nature of radiating elements. An innovative approach is exploited to synthesis harmonic patterns with high sideband level within the 'blind' directions of the element factor. A set of representative numerical results is reported to illustrate the potentialities and the limitations of the proposed approach considering both sum and difference patterns.

Numerical Validation

TEST CASE 2 - 0.5λ Elements Spacing - Short Dipoles - Dolph Pattern

Goal

Sideband radiation minimization of a TMLA composed by real radiating elements (short dipoles considered in this test case) adopting the pulse shifting technique.

Test Case Description

- Number of Elements: N = 16
- Elements Spacing: $d = 0.5\lambda$
- Static Array Configuration: $\alpha_n = 1, n = 0, ..., N 1$
- Pattern at Central Frequency: Dolph Chebyshev, $SLL = -30 \, dB$
- Max Gain Pattern Direction : $\theta^{max}=90^\circ$

1.b) Optimization Approach: PS-PSO, SR Min.

The optimization process though the PSO algorithm acts just on the temporal shift of the pulses;

- Number of Variables: X = 16
- Number of Particles: S = 15 30
- Number of Iterations: I = 500
- Inertial Weight: Linearly varying: 0.9 to 0.4
- Cost Function:

$$\Psi^{PSO}\left[\tau_n'(i_k)\right] = P_{SR}^{act,(i_k)} \tag{1}$$

Dolph-Chebyshev Pattern, SLL=-30 dB - Original - Short Dipole Elements Array



Fig.17 - Pulse Sequence



Fig.18 - Isotropic - Pattern(u)



Fig.19 - Short Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - End-Fire h=1 - Short Dipole Elements Array



Fig.20 - Pulse Sequence



Fig.21 - Isotropic - Pattern(u)



Fig.22 - Short Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=1 - Short Dipole Elements Array



Fig.23 - Pulse Sequence



Fig.24 - Isotropic - Pattern(u)



Fig.25 - Short Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=2 - Short Dipole Elements Array



Fig.26 - Pulse Sequence



Fig.27 - Isotropic - Pattern(u)



Fig.28 - Short Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=100 - Short Dipole Elements Array



Fig.29 - Pulse Sequence



Fig.30 - Isotropic - Pattern(u)



Fig.31 - Short Dipole - Pattern(u)

	$SLL\left[dB ight]$	$SBL\left[dB ight]$	$SBL_1[dB]$	$SBL_2\left[dB\right]$	$BW\left[deg ight]$	SR[%]
Dolph-Chebyshev	-30.08	-12.39	-12.39	-18.30	15.85	22.50
EndFireh=1Pattern	-30.08	-18.30	-20.12	-18.30	15.85	12.18
PS - PSO, SRMin. H = 1	-30.08	-19.65	-19.65	-19.75	15.85	11.45
PS - PSO, SRMin. H = 2	-30.08	-19.29	-19.29	-21.28	15.85	11.45
PS - PSO, SRMin. H = 100	-30.08	-19.44	-19.44	-19.47	15.85	11.45

Tab.2 - Sidelobe Lebel (SLL), Sideband Level (SBL), -3 dB Beamwidth (BW), Sideband Radiation (SR).

TEST CASE 3 - 0.7λ Elements Spacing - Dipoles - Dolph Pattern

Goal

Sideband radiation minimization of a TMLA composed by real radiating elements (dipoles considered in this test case) adopting the pulse shifting technique.

Test Case Description

- Number of Elements: N = 16
- Elements Spacing: $d = 0.7\lambda$
- Static Array Configuration: $\alpha_n = 1, \ n = 0, ..., N 1$
- Pattern at Central Frequency: Dolph Chebyshev, $SLL = -30 \, dB$
- Max Gain Pattern Direction : $\theta^{max}=90^\circ$

1.b) Optimization Approach: PS-PSO, SR Min.

The optimization process though the PSO algorithm acts just on the temporal shift of the pulses;

- Number of Variables: X = 16
- Number of Particles: S = 15 30
- Number of Iterations: I = 500
- Inertial Weight: Linearly varying: 0.9 to 0.4
- Cost Function:

$$\Psi^{PSO}\left[\tau_n'(i_k)\right] = P_{SR}^{act,(i_k)}$$

(2)

Dolph-Chebyshev Pattern, SLL=-30 dB - Original - Dipole Elements Array



Fig.32 - Pulse Sequence

-10

-20

-30

-4(

-50

-1 -0.8 -0.6 -0.4 -0.2



Fig.33 - Isotropic - Pattern(u)



0 $u = \cos\theta$

0.2 0.4 0.6 0.8

q=0 |q|=1 |q|=2

Dolph-Chebyshev Pattern, SLL=-30 dB - End-Fire h=1 - Dipole Elements Array



Fig.35 - Pulse Sequence



Fig.36 - Isotropic - Pattern(u)



Fig.37 - Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=1 - Dipole Elements Array



Fig.38 - Pulse Sequence



Fig.39 - Isotropic - Pattern(u)



Fig.40 - Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=2 - Dipole Elements Array



Fig.41 - Pulse Sequence



Fig.42 - Isotropic - Pattern(u)



Fig.43 - Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=100 - Dipole Elements Array



Fig.44 - Pulse Sequence



Fig.45 - Isotropic - Pattern(u)



Fig.46 - Dipole - Pattern(u)

	$SLL\left[dB ight]$	$SBL\left[dB ight]$	$SBL_1[dB]$	$SBL_2\left[dB\right]$	BW[deg]	SR[%]
Dolph-Chebyshev	-30.02	-12.39	-12.39	-18.30	11.33	23.28
End Fire h = 1 Pattern	-30.02	-13.64	-13.64	-20.68	11.33	20.63
PS - PSO, SRMin. H = 1	-30.02	-13.31	-13.31	-19.21	11.33	20.37
PS - PSO, SRMin. H = 2	-30.02	-13.78	-13.78	-20.82	11.33	20.22
PS - PSO, SRMin. H = 100	-30.02	-13.82	-13.82	-19.64	11.33	20.16

Tab.3 - Sidelobe Lebel (SLL), Sideband Level (SBL), -3 dB Beamwidth (BW), Sideband Radiation (SR).

TEST CASE 4 - 0.4λ Elements Spacing - Short Dipoles - Dolph Pattern

Goal

Sideband radiation minimization of a TMLA composed by real radiating elements (short dipoles considered in this test case) adopting the pulse shifting technique.

Test Case Description

- Number of Elements: N = 16
- Elements Spacing: $d = 0.4\lambda$
- Static Array Configuration: $\alpha_n = 1, n = 0, ..., N 1$
- Pattern at Central Frequency: Dolph Chebyshev, $SLL = -30 \, dB$
- Max Gain Pattern Direction : $\theta^{max}=90^\circ$

1.b) Optimization Approach: PS-PSO, SR Min.

The optimization process though the PSO algorithm acts just on the temporal shift of the pulses;

- Number of Variables: X = 16
- Number of Particles: S = 15 30
- Number of Iterations: I = 500
- Inertial Weight: Linearly varying: 0.9 to 0.4
- Cost Function:

$$\Psi^{PSO}\left[\tau_n'(i_k)\right] = P_{SR}^{act,(i_k)}$$

(3)

Dolph-Chebyshev Pattern, SLL=-30 dB - Original - Short Dipole Elements Array



Fig.47 - Pulse Sequence



Fig.48 - Isotropic - Pattern(u)



Fig.49 - Short Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - End-Fire h=1 - Short Dipole Elements Array



Fig.50 - Pulse Sequence



Fig.51 - Isotropic - Pattern(u)



Fig.52 - Short Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=1 - Short Dipole Elements Array



Fig.53 - Pulse Sequence



Fig.54 - Isotropic - Pattern(u)



Fig.55 - Short Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=2 - Short Dipole Elements Array



Fig.56 - Pulse Sequence



Fig.57 - Isotropic - Pattern(u)



Fig.58 - Short Dipole - Pattern(u)

Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=100 - Short Dipole Elements Array



Fig.59 - Pulse Sequence



Fig.60 - Isotropic - Pattern(u)



Fig.61 - Dipole - Pattern(u)

	$SLL\left[dB ight]$	$SBL\left[dB ight]$	$SBL_1\left[dB\right]$	$SBL_2\left[dB\right]$	BW[deg]	SR[%]
Dolph-Chebyshev	-30.20	-12.38	-12.38	-18.30	19.78	21.69
End Fire h = 1 Pattern	-30.20	-19.26	-19.26	-19.54	19.78	9.17
PS - PSO, SRMin. H = 1	-30.20	-19.20	-30.15	-19.20	19.78	7.81
PS - PSO, SRMin. H = 2	-30.20	-20.59	-23.62	-20.59	19.78	7.73
PS - PSO, SRMin. H = 100	-30.20	-19.63	-19.63	-27.15	19.78	7.62

Tab.4 - Sidelobe Lebel (SLL), Sideband Level (SBL), -3 dB Beamwidth (BW), Sideband Radiation (SR).

TEST CASE 5 - 0.7λ Elements Spacing - Dipoles on Ground Plane - Dolph Pattern

Goal

Sideband radiation minimization of a TMLA composed by real radiating elements (short dipoles considered in this test case) adopting the pulse shifting technique.

Test Case Description

- Number of Elements: N = 16
- Elements Spacing: $d = 0.7\lambda$
- Static Array Configuration: $\alpha_n = 1, n = 0, ..., N 1$
- Pattern at Central Frequency: Dolph Chebyshev, SLL = -30 dB
- Max Gain Pattern Direction : $\theta^{max} = 90^{\circ}$
- Dipole Length: $l = 0.5\lambda$
- Dipole Distance from Ground Plane: $h=0.75\lambda$
- Ground Plane Dimension: $8\lambda\times 8\lambda$

1.b) Optimization Approach: PS-PSO, SR Min.

The optimization process though the PSO algorithm acts just on the temporal shift of the pulses;

- Number of Variables: X = 16
- Number of Particles: S = 15
- Number of Iterations: I = 500
- Inertial Weight: Linearly varying: 0.9 to 0.4
- Cost Function:

$$\Psi^{PSO}\left[\tau_n'(i_k)\right] = P_{SR}^{act,(i_k)} \tag{4}$$



Fig.62 - Element Factor

Dolph-Chebyshev Pattern, SLL=-30 dB - Original - Dipoles on a Ground Plane



Dolph-Chebyshev Pattern, SLL=-30 dB - End-Fire h=1 - Dipoles on a Ground Plane





Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=1 - Dipoles on a Ground Plane



Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=2 - Dipoles on a Ground Plane







Dolph-Chebyshev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=100 - Dipoles on a Ground Plane



Fig.71 - Pulse Sequence



Fig.72 - Dipole - Pattern(u)

	$SLL\left[dB ight]$	$SBL\left[dB ight]$	$SBL_1[dB]$	$SBL_2\left[dB\right]$	BW[deg]	SR[%]
Dolph-Chebyshev	-30.24	-12.38	-12.38	-18.30	19.78	22.23
End Fire h = 1 Pattern	-30.24	-14.77	-14.77	-24.20	19.78	15.58
PS - PSO, SRMin. H = 1	-30.24	-19.11	-21.70	-19.11	19.78	10.62
PS - PSO, SRMin. H = 2	-30.24	-21.41	-22.14	-21.41	19.78	10.61
PS - PSO, SRMin. H = 100	-30.24	-20.09	-22.19	-20.09	19.78	10.59

Tab.5 - Sidelobe Lebel (SLL), Sideband Level (SBL), -3 dB Beamwidth (BW), Sideband Radiation (SR).

TEST CASE 6 - 0.5λ Elements Spacing - Short Dipoles - Zolotarev Pattern

Goal

Sideband radiation minimization of a TMLA composed by real radiating elements (short dipoles considered in this test case) adopting the pulse shifting technique.

Test Case Description

- Number of Elements: N = 16
- Elements Spacing: $d = 0.5\lambda$
- Static Array Configuration: $\alpha_n = 1, \ n = 0, ..., N 1$
- Pattern at Central Frequency: Zolotarev, $SLL = -30 \, dB$
- Dipole Length: $l = 0.5\lambda$

1.b) Optimization Approach: PS-PSO, SR Min.

The optimization process though the PSO algorithm acts just on the temporal shift of the pulses;

- Number of Variables: X = 16
- Number of Particles: S = 15
- Number of Iterations: I = 500
- Inertial Weight: Linearly varying: 0.9 to 0.4
- Cost Function:

$$\Psi^{PSO}\left[\tau_n'(i_k)\right] = P_{SR}^{act,(i_k)} \tag{5}$$

Zolotarev Pattern, SLL=-30 dB - Original - Short Dipole Elements Array



Fig.75 - Pulse Sequence



Fig.76 - Isotropic - Pattern(u)



Fig.77 - Short Dipole - Pattern(u)

Zolotarev Pattern, SLL=-30 dB - End-Fire h=1 - Short Dipole Elements Array



Fig.78 - Pulse Sequence



Fig.79 - Isotropic - Pattern(u)



Fig.80 - Short Dipole - Pattern(u)

Zolotarev Pattern, SLL=-30 dB - Analytic Steering (Maximum of h=1 harmonic pattern in End-Fire) - Short Dipole Elements Array







Fig.82 - Isotropic - Pattern(u)



Fig.83 - Short Dipole - Pattern(u)

Zolotarev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=1 - Short Dipole Elements Array



Fig.84 - Pulse Sequence



Fig.85 - Isotropic - Pattern(u)



Fig.86 - Short Dipole - Pattern(u)

Zolotarev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=2 - Short Dipole Elements Array



Fig.87 - Pulse Sequence



Fig.88 - Isotropic - Pattern(u)



Fig.89 - Short Dipole - Pattern(u)

Zolotarev Pattern, SLL=-30 dB - PS-PSO, SR Min. H=100 - Short Dipole Elements Array





Fig.91 - Isotropic - Pattern(u)



Fig.92 - Dipole - Pattern(u)

	$SLL\left[dB ight]$	$SBL\left[dB ight]$	$SBL_1[dB]$	$SBL_2\left[dB\right]$	$BW\left[deg ight]$	SR[%]
Zolotarev	-30.03	-13.67	-13.67	-20.19	6.5	19.60
End - Fire h = 1 Pattern	-30.03	-16.36	-16.36	-20.19	6.5	14.49
Analytic Steering End - Fire Max h = 1	-30.03	-15.73	-15.73	-20.18	6.5	14.91
PS - PSO, SRMin. H = 1	-30.03	-17.89	-17.89	-21.64	6.5	11.41
PS - PSO, SRMin. H = 2	-30.03	-17.57	-17.57	-22.91	6.5	11.41
PS - PSO, SRMin. H = 100	-30.03	-17.14	-17.14	-22.89	6.5	11.45

Tab.6 - Sidelobe Lebel (SLL), Sideband Level (SBL), -3 dB Beamwidth (BW), Sideband Radiation (SR).

References

- L. Manica, P. Rocca, L. Poli, and A. Massa, "Almost time-independent performance in time-modulated linear arrays," vol. 8, pp. 843-846, 2009.
- [2] P. Rocca, L. Poli, G. Oliveri, and A. Massa, "A multi-stage approach for the synthesis of sub-arrayed time modulated linear arrays," IEEE Trans. Antennas Propag., vol. 59, no. 9, pp. 3246-3254, Sep. 2011.
- [3] L. Poli, P. Rocca, G. Oliveri, and A. Massa, "Harmonic beamforming in time-modulated linear arrays," IEEE Trans. Antennas Propag., vol. 59, no. 7, pp. 2538-2545, Jul. 2011.
- [4] L. Poli, P. Rocca, L. Manica, and A. Massa, "Handling sideband radiations in time-modulated arrays through particle swarm optimization," IEEE Trans. Antennas Propag., vol. 58, no. 4, pp. 1408-1411, Apr. 2010.
- [5] P. Rocca, L. Poli, and A. Massa, "Instantaneous directivity optimization in time-modulated array receivers," IET Microwaves, Antennas & Propagation, vol. 6, no. 14, pp. 1590-1597, Nov. 2012.
- [6] L. Poli, P. Rocca, and A. Massa, "Sideband radiation reduction exploiting pattern multiplication in directive time-modulated linear arrays," IET Microwaves, Antennas & Propagation, vol. 6, no. 2, pp. 214-222, 2012.
- [7] L. Poli, P. Rocca, G. Oliveri, and A. Massa, "Adaptive nulling in time-modulated linear arrays with minimum power losses," IET Microwaves, Antennas & Propagation, vol. 5, no. 2, pp. 157-166, 2011.
- [8] L. Poli, P. Rocca, L. Manica, and A. Massa, "Time modulated planar arrays Analysis and optimization of the sideband radiations," IET Microwaves, Antennas & Propagation, vol. 4, no. 9, pp. 1165-1171, 2010.
- [9] L. Poli, P. Rocca, L. Manica, and A. Massa, "Pattern synthesis in time-modulated linear arrays through pulse shifting," IET Microwaves, Antennas & Propagation, vol. 4, no. 9, pp. 1157-1164, 2010.
- [10] P. Rocca, L. Poli, G. Oliveri, and A. Massa, "Synthesis of time-modulated planar arrays with controlled harmonic radiations," Journal of Electromagnetic Waves and Applications, vol. 24, no. 5/6, pp. 827-838, 2010.
- [11] P. Rocca, L. Manica, L. Poli, and A. Massa, "Synthesis of compromise sum-difference arrays through time-modulation," IET Radar, Sonar & Navigation, vol. 3, no. 6, pp. 630-637, 2009.
- [12] P. Rocca, Q. Zhu, E. T. Bekele, S. Yang, and A. Massa, "4D arrays as enabling technology for cognitive radio systems," IEEE Transactions on Antennas and Propagation - Special Issue on "Antenna Systems and Propagation for Cognitive Radio," vol. 62, no. 3, pp. 1102-1116, Mar. 2014.